## 10 SITV:3:4T

RENTALS

## Datasheet



03703306021
www.sunbeltrentals.co.uk

## Recorder and analyser for measurements on electrical power networks

## Technical Specifications

The QualistarPlus C.A 8335 is synonymous with simplicity, performance, versatility and powerful analysis.
It offers all the necessary functions with demanding specifications usually reserved for top-of-the-range laboratory instruments
This instrument is ideal for engineers and technicians seeking all the functions of an electrical network analyser in a portable, battery-powered instrument.

- Real-time display of wave forms (4 voltages and 4 currents)
- RMS voltage and currents per half-period
- Intuitive use
- Automatic recognition of the different types of current sensors
- Integration of all the DC components
- Measurement, calculation and display of the harmonics up to the 50th order, along with the phase information
- Calculation of Total Harmonic Distortion (THD)
- Capture of transients per sample $\left(1 / 256^{\text {th }}\right.$ of a period)
- Display of phasor diagram
- Measurement of VA, W and var power values (total and per phase)
- Measurement of VAh, Wh and varh energy values (total and per phase)
- Calculation of the K-Factor
- Calculation of the $\cos \varphi$ displacement power factor (DPF) and the power factor (PF)
- Capture of up to 300 transients
- Flicker calculation
- Unbalance calculation (current and voltage)
- Monitoring of the electrical network with setting of alarms
- Back-up and recording of screenshots (image and data)
- Software for data recovery and real-time communication with a PC
- Recording and export onto PC


## 1. GENERAL SPECIFICATIONS

### 1.1. Casing

| Casing: | Rigid moulded casing overmoulded with a yellow thermo-adhesive elastomer. |
| :---: | :---: |
| Connectors: | 5 voltage measurement sockets. |
|  | 4 special current connectors (automatic recognition of clamp-on ammeters). |
|  | A connector for the specific mains power supply. |
|  | A connector for the USB link. |
|  | A connector for the SD memory card. This is located in the compartment on the back of the C.A 8335, under the rechargeable batteries. |
| Keys: | For functions, navigation and mode changes. Designed to allow use with gloves. |
| Metal ring: | Located on the back of the C.A 8335. It can be used to attach the instrument with a padlock. |
| Stand: | To keep the instrument at an angle of $53^{\circ}$ in relation to the horizontal. |
| Compartment: | For access to the rechargeable batteries at the rear of the instrument. |
| Dimensions: | Total: $200 \times \mathrm{H} 250 \times \mathrm{P} 67$ |
|  | Screen: $320 \times 240$ pixels W $118 \mathrm{~mm} \times \mathrm{H} 90 \mathrm{~mm}$ diagonal 148 mm |
| Weight: | 1.950 g (with rechargeable batteries) |

### 1.2. Power supply

### 1.2.1. Mains power supply

| Type: | Specific external mains power <br> supply: 600 Vrms category IV - <br> 1,000 |
| :--- | :--- |
| Opms category III <br> range: | $230 \mathrm{~V} \pm 10 \% @ 50 \mathrm{~Hz}$ and 120 V |
| Max. power: | 40 VA |

### 1.2.2. Battery power supply

The C.A 8335 can be used without a mains power supply. The battery also allows the Qualistar+ to be used in the event of mains power cuts.

| Battery: | 8 rechargeable NiMH batteries |
| :--- | :--- |
| Capacity: | minimum $4,000 \mathrm{mAh}$ |
| Rated voltage: | 1.2 V per element, 9.6 V in total |
| Life span: | at least 500 recharge-discharge cycles |
| Recharge <br> current: | 1 A |
| Recharge time: | Approximately 5 hours |
| Operating $\mathrm{T}^{\circ}:$ | $\left[0^{\circ} \mathrm{C} ; 50^{\circ} \mathrm{C}\right]$ |
| Recharge $\mathrm{T}^{\circ}$ | $\left[10^{\circ} \mathrm{C} ; 40^{\circ} \mathrm{C}\right]$ |
| Storage $\mathrm{T}^{\circ}:$ | Storage for $\leq 30$ days: <br> $\left[-20^{\circ} \mathrm{C} ;+50^{\circ} \mathrm{C}\right]$ |
|  | Storage for 30 to 90 days: <br> $\left[-20^{\circ} \mathrm{C} ;+40^{\circ} \mathrm{C}\right]$ |

1.2.3 Consumption

| With $50 \%$ brightness: | 300 mA |
| :--- | :--- |
| Standby mode without display: | 100 mA |

### 1.3 Operating range

### 1.3.1 Environmental conditions

1.3.1.1 Climatic conditions

The ambient temperature and humidity requirements are shown in the graph below:


1 = Range of reference
2 = Operating range
Caution: above $40{ }^{\circ} \mathrm{C}$, the instrument must be used EITHER with the "battery only" OR with the "specific external mains power pack only" - use of the instrument with the battery AND the specific external mains power pack simultaneously is prohibited.
3 = Storage range with batteries
4 = Storage range without batteries

### 1.3.1.2 Altitude

Operation: [ $0 \mathrm{~m} ; 2000 \mathrm{~m}$ ]
Storage: [0 m ; 10000 m ]

### 1.3.2 Mechanical conditions

According to the IEC 61010-1 standard, the C.A 8335 is considered to be a PORTABLE (HANDHELD) INSTRUMENT.

- Operating position: any position.
- Position of reference in operation: on a horizontal surface, fitted on its stand or placed flat.
- Rigidity (IEC 61010-1): 30 N force applied to the whole of the instrument, with the instrument maintained in place (test carried out at $40^{\circ} \mathrm{C}$ ).
- Falls (IEC 61010-1): 1 m in the position supposed to be the most severe; the acceptance criterion for falls is: no permanent mechanical damage and no functional deterioration.
- Leakproofing: IP 50 as per NF EN 60529 A1 (electrical IP2X for the terminals).


### 1.3.3 Electromagnetic compatibility

### 1.3.3.1 Immunity according to NF EN 61326-1 A3

- Resistance to electrostatic discharges (as per IEC 61000-4-2)
Level 1 : Severity : 4 kV in contact Acceptance : CRITERION A
Level 2 : Severity $: 8 \mathrm{kV}$ in the air Acceptance: CRITERION A
- Resistance to radiated fields (as per IEC 61000-4-3 and IEC 61000-4-8)
Severity: 10 V.m ${ }^{-1}$
Acceptance: CRITERION B (THD ${ }_{\mathrm{A}}$ altered on the Rogowski line)
- Resistance to fast transients (as per IEC 61000-4-4)

Severity:
2 kV on the voltage inputs and on the power supply
1 kV on the current inputs
Acceptance: CRITERION A

- Resistance to electric shocks (as per IEC 61000-4-5)

Severity:
2 kV on the voltage inputs in differential mode 1 kV on the voltage inputs in common mode Acceptance: CRITERION A

- Conducted RF disturbances (as per IEC 61000-4-6)

Severity: 3 V on the voltage inputs and on the power supply Acceptance: CRITERION A

- Voltage interruption (as per IEC 61000-4-11)

Severity: $100 \%$ de perte sur une période de l'alimentation Acceptance: CRITERION A
1.3.3.2 Emissions according to NF EN 61326-1 A3

- Class A equipment (without power supply - mains power pack).
- Class B equipment (with power supply - mains power pack - power-pack lead is involved).


### 1.4 User safety

- Application of the safety rules in compliance with IEC 61010-1. (Insulation between voltage inputs by protective impedances).
- Pollution degree 2.
- Installation category IV*, operating voltage $600 \mathrm{~V}_{\mathrm{RMS}}$.
- Dual insulation on the $\mathrm{I} / \mathrm{Os}$ in relation to the earth (回symbol).
- Dual insulation between the voltage inputs, the power supply and the other I/Os ( $\square$ symbol).
- Indoor use
(*) Caution: the rated voltage and measurement category of the overall "instrument + current sensor" assembly may differ from the specifications of the instrument alone.
- use of the AmpFLEX ${ }^{\text {TM }}$, MiniFLEX and C clamps maintains the rating of the overall "instrument + current sensor" assembly at $\mathbf{6 0 0}$ V Category IV or $\mathbf{1 , 0 0 0}$ V Category III.
- use of the PAC, MN93 and MN93A clamps downgrades the overall "instrument + current sensor" assembly to 300 V Category IV or $\mathbf{6 0 0}$ V Category III.
- use of the 5 A adapter box downgrades the overall "instrument + current sensor" assembly to 150 V Category IV or 300 V Category III.


## 2. FUNCTIONAL SPECIFICATIONS

### 2.1 Conditions of reference

This table shows the conditions of reference for the quantities to be used by default in the specifications provided in §2.2.4.

| Influencing quantity | Conditions of reference |
| :---: | :---: |
| Ambient temperature | $23^{\circ} \mathrm{C} \pm 3 \mathrm{~K}$ |
| Relative humidity | [45 \% ; 75 \%] |
| Atmospheric pressure | [860 hPa ; 1060 hPa ] |
| Phase voltage | [ $50 \mathrm{~V}_{\text {RMS } ;} 1,000 \mathrm{~V}_{\text {RMS }}$ ] without DC ( $<0.5 \%$ ) |
| Input voltage of standard current circuit | $\begin{aligned} & {\left[30 \mathrm{mV}_{\mathrm{RMS}} ; 1 \mathrm{~V}_{\mathrm{RMS}}\right] \text { without } \mathrm{DC}(<0.5 \%)} \\ & \text { N.B. } \mathrm{I}_{\text {rated }} \Leftrightarrow 1 \mathrm{~V}_{\mathrm{RMS}} \text { and } 3 \times \mathrm{I}_{\text {rated }} \div 100 \Leftrightarrow 30 \mathrm{mV}_{\mathrm{RMS}} \\ & {\left[11.73 \mathrm{mV}_{\mathrm{RMS}} ; 117.3 \mathrm{mV}_{\mathrm{RMS}}\right] \text { without } \mathrm{DC}(<0.5 \%)} \end{aligned}$ |
| Input voltage of Rogowski current circuit | $\begin{aligned} & \mathrm{I}_{\text {rated }} \Leftrightarrow 117.3 \mathrm{mV}_{\text {RMS }} \text { at } 50 \mathrm{~Hz} \\ & \mathrm{I}_{\text {rated }} \div 10 \Leftrightarrow 11.73 \mathrm{mV}_{\text {RMS }} \text { at } 50 \mathrm{~Hz} \end{aligned}$ |
| Electrical network frequency | $50 \mathrm{~Hz} \pm 0,1 \mathrm{~Hz}$ and $60 \mathrm{~Hz} \pm 0.1 \mathrm{~Hz}$ |
| Phase shift | $0^{\circ}$ (active power) and $90^{\circ}$ (reactive power) |
| Harmonics | < 0.1 \% |
| Voltage unbalance | < 10 \% |

### 2.2 Electrical specifications

### 2.2.1 Voltage input specifications

| Operating <br> range: | $0 \mathrm{~V}_{\text {RMS }}$ to $1,000 \mathrm{~V}_{\mathrm{RMS}} \mathrm{AC}+\mathrm{DC}$ <br> phase-neutral and neutral-earth |
| :--- | :--- |
|  | $0 \mathrm{~V}_{\text {RMS }}$ to $2,000 \mathrm{~V}_{\mathrm{RMS}} \mathrm{AC}+\mathrm{DC}$ <br> phase-phase <br> (subject to compliance with 1,000 $\mathrm{V}_{\mathrm{RMS}}$ <br> in relation to the earth in Category III) |
| Input <br> impedance: | $969 \mathrm{k} \Omega$ (between phase and neutral <br> and between neutral and earth) |
| Admissible <br> overload: | $1.2 \times \mathrm{V}_{\text {rated }}$ permanently |
|  | $2 \times \mathrm{V}_{\text {rated }}$ for 1 second. |

### 2.2.2 Current input specifications

| Operating range: | $[0 \mathrm{~V} ; 1 \mathrm{~V}]$ |
| :--- | :--- |
| Input impedance: | $1 \mathrm{M} \Omega$. |
| Admissible overload: | 1.7 V. |

The AmpFLEX ${ }^{\text {TM }}$ configuration switches the current input onto an integrating assembly (Rogowski line) capable of interpreting the signals delivered by the AmpFLEX ${ }^{\text {m }}$ sensors. In this case, the input impedance is reduced to $12.4 \mathrm{k} \Omega$.

### 2.2.3 Bandwidth

| Measurement <br> channels: | 256 counts per period, i.e.: |
| :--- | :--- |
|  |  |
|  | For $50 \mathrm{~Hz}: 6.4 \mathrm{kHz}$ |
| $(256 \times 50 \div 2)$ |  |
|  | For $60 \mathrm{~Hz}: 7.68 \mathrm{kHz}$ |
| $(256 \times 60 \div 2)$ |  |
| Analogue at $-3 \mathrm{~dB}:$ | $>10 \mathrm{kHz}$ |

## Power \& Quality Analyser C.A 8335

### 2.2.4 Specifications of instrument alone (excluding current sensor)

The information which follows corresponds to a situation involving "ideal current sensors" (perfect linearity with no phase shift). The current specifications (and derived quantities) are stipulated, respectively, for each of the two configurations: "without AmpFLEX ${ }^{\text {TM }}$ \& MiniFLEX " and "with AmpFLEX ${ }^{\text {TM }}$ \& MiniFLEX".

| Measurement |  | Measurement range |  | Display resolution | Maximum error in reference range |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Minimum | Maximum |  |  |
| Frequency |  | 40 Hz | 69 Hz | $0,01 \mathrm{~Hz}$ | $\pm(1 \mathrm{ct})$ |
| TRMS phase voltage |  | 10 V | 1,000 $\mathrm{V}^{(1)}$ | $\begin{gathered} 0.1 \mathrm{~V} \\ \mathrm{~V}<1,000 \mathrm{~V} \end{gathered}$ | $\pm(0.5$ \% + 2 cts ) |
|  |  | $\begin{gathered} 1 \mathrm{~V} \\ \mathrm{~V} \geq 1,000 \mathrm{~V} \end{gathered}$ |  | $\pm(0.5 \%+1 \mathrm{ct})$ |  |
| TRMS composite voltage |  |  | 10 V | 2,000 V ${ }^{(2)}$ | $\begin{gathered} 0.1 \mathrm{~V} \\ \mathrm{~V}<1,000 \mathrm{~V} \\ \hline \end{gathered}$ | $\pm(0.5$ \% + 2 cts ) |
|  |  | $\begin{gathered} 1 \mathrm{~V} \\ \mathrm{~V} \geq 1,000 \mathrm{~V} \end{gathered}$ |  |  | $\pm(0.5$ \% + 1 ct$)$ |
| DC voltage |  | 10 V | 1,000 V | $\begin{gathered} 0.1 \mathrm{~V} \\ \mathrm{~V}<1,000 \mathrm{~V} \\ \hline \end{gathered}$ | $\pm(1 \%+5 \mathrm{cts})$ |
|  |  | $\begin{gathered} 1 \mathrm{~V} \\ \mathrm{~V} \geq 1,000 \mathrm{~V} \end{gathered}$ |  | $\pm(1 \%+1 \mathrm{ct})$ |  |
| TRMS current | Without AmpFLEX ${ }^{\text {™ }}$ \& Mini-AmpFLEX |  | $I_{\text {rated }} \div 1,000$ <br> [A] | $1.2 \times \mathrm{I}_{\text {rated }}$ <br> [A] | $\begin{gathered} 0,1 \mathrm{~A} \\ \mathrm{I}<1,000 \mathrm{~A} \end{gathered}$ | $\pm(0.5$ \% + 2 cts ) |
|  |  | $\begin{gathered} 1 \mathrm{~A} \\ \mathrm{I} \geq 1,000 \mathrm{~A} \end{gathered}$ |  |  | $\pm(0.5$ \% + 1 ct$)$ |
|  | $\begin{gathered} \text { AmpFLEX }{ }^{\text {TM }} \\ \& \\ \text { Mini-AmpFLEX } \end{gathered}$ | 10 A | 6,500 A | $\begin{gathered} 0,1 \mathrm{~A} \\ \mathrm{I}<1,000 \mathrm{~A} \end{gathered}$ | $\pm(0.5 \%+1 \mathrm{~A})$ |
|  |  |  |  | $\begin{gathered} 1 \mathrm{~A} \\ \mathrm{I} \geq 1,000 \mathrm{~A} \end{gathered}$ |  |
| DC current |  | 1 A | 1,200 $\mathrm{A}^{(3)}$ | $\begin{gathered} 0,1 \mathrm{~A} \\ \mathrm{I}<1,000 \mathrm{~A} \end{gathered}$ | $\pm(1 \%+1 \mathrm{~A})$ |
|  |  | $\begin{gathered} 1 \mathrm{~A} \\ \mathrm{I} \geq 1,000 \mathrm{~A} \end{gathered}$ |  |  |  |
| Peak current |  |  | $I_{\text {rated }} \div 1,000$ <br> [A] | $\begin{gathered} 1.7 \times I_{\text {rated }} \\ {[A]^{(4)}} \end{gathered}$ | $\begin{gathered} 0,1 \mathrm{~A} \\ \mathrm{I}<1,000 \mathrm{~A} \end{gathered}$ | $\pm(1 \%+1 \mathrm{~A})$ |
|  |  <br> Mini-AmpFLEX | 10 A | 9,190 $\mathrm{A}^{(5)}$ | $\begin{gathered} 1 \mathrm{~A} \\ \mathrm{I} \geq 1,000 \mathrm{~A} \end{gathered}$ |  |  |
| Half-period TRMS current ${ }^{(7)}$ | Without AmpFLEX ${ }^{\text {TM }}$ | $I_{\text {rated }} \div 100$ <br> [A] | $1.2 \times \mathrm{I}_{\text {rated }}$ <br> [A] | $\begin{gathered} 0,1 \mathrm{~A} \\ \mathrm{I}<1,000 \mathrm{~A} \\ \hline \end{gathered}$ | $\pm(1 \%+1 \mathrm{~A})$ |  |
|  | Mini-AmpFLEX |  |  | $\begin{gathered} 1 \mathrm{~A} \\ \mathrm{I} \geq 1,000 \mathrm{~A} \end{gathered}$ |  |  |
|  | $\begin{gathered} \text { AmpFLEX } \\ \& \\ \text { Mini-AmpFLEX } \end{gathered}$ | 100 A | 6,500 A | $\begin{gathered} 0,1 \mathrm{~A} \\ \mathrm{I}<1,000 \mathrm{~A} \end{gathered}$ | $\pm(1.5 \%+4 \mathrm{~A})$ |  |
|  |  |  |  | $\begin{gathered} 1 \mathrm{~A} \\ \mathrm{I} \geq 1,000 \mathrm{~A} \end{gathered}$ |  |  |
| Peak phase voltage |  | 10 V | 1,414 $\mathrm{V}^{(6)}$ | $\begin{gathered} 0.1 \mathrm{~V} \\ \mathrm{~V}<1,000 \mathrm{~V} \end{gathered}$ | $\pm(1 \%+1 \mathrm{~V})$ |  |
|  |  | $\begin{gathered} 1 \mathrm{~V} \\ \mathrm{~V} \geq 1,000 \mathrm{~V} \end{gathered}$ |  |  |  |  |
| Peak composite voltage |  |  | 10 V | 2,828 $\mathrm{V}^{(7)}$ | $\begin{gathered} 0.1 \mathrm{~V} \\ \mathrm{U}<1,000 \mathrm{~V} \\ \hline \end{gathered}$ | $\pm(1 \%+1 \mathrm{~V})$ |
|  |  | $\begin{gathered} 1 \mathrm{~V} \\ \mathrm{U} \geq 1,000 \mathrm{~V} \end{gathered}$ |  |  |  |  |

(1) Rating $1,000 \mathrm{~V}_{\text {RMS }}$ Category III, as long as the voltages between each of the terminals and the earth do not exceed $1,000 \mathrm{~V}_{\text {RMs }}$.
(2) With two-phase (opposing phases) - same remark as for (1).
(3) Limitation of the PAC clamp.
(4) $1.2 \times$ Irated $\times \sqrt{2}=1.7 \times$ Irated
(5) $6,500 \times \sqrt{2}=9,190$
(6) $1,000 \times \sqrt{2}=1,414$
(7) $2000 \times \sqrt{2}=2828$

## Power \& Quality Analyser C.A 8335

| Measurement |  | Measurement range |  | Display resolution | Maximum error in reference range |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Minimum | Maximum |  |  |
| Half-period TRMS phase voltage ${ }^{(3)}$ |  | 10 V | 1,000 ${ }^{(1)}$ | $\begin{gathered} 0.1 \mathrm{~V} \\ \mathrm{~V}<1,000 \mathrm{~V} \end{gathered}$ | $\pm(0.8 \%+1 \mathrm{~V})$ |
|  |  | $\begin{gathered} 1 \mathrm{~V} \\ \mathrm{~V} \geq 1,000 \mathrm{~V} \end{gathered}$ |  |  |  |
| Half-period TRMS composite voltage ${ }^{(3)}$ |  |  | 10 V | 2,000 ${ }^{(2)}$ | $\begin{gathered} 0.1 \mathrm{~V} \\ \mathrm{U}<1,000 \mathrm{~V} \end{gathered}$ | $\pm(0.8 \%+1 \mathrm{~V})$ |
|  |  | $\begin{gathered} 1 \mathrm{~V} \\ \mathrm{U} \geq 1,000 \mathrm{~V} \end{gathered}$ |  |  |  |  |
| Crest factor |  | 1 | 3.99 | 0.01 | $\pm(1 \%+2 \mathrm{cts})$ |  |
|  |  | 4 | 9.99 | 0.01 | $\pm(5 \%+2 \mathrm{cts})$ |  |
| Puissance active | $\begin{gathered} \text { Without } \\ \text { AmpFLEX } \\ \& \\ \text { Mini-AmpFLEX } \end{gathered}$ | 0 W | 9,999 kW | $\begin{gathered} 1 \mathrm{~V} \\ \mathrm{U} \geq 1,000 \mathrm{~V} \end{gathered}$ | $\begin{gathered} \pm(1 \%) \\ \operatorname{Cos} \phi \geq 0.8 \end{gathered}$ |  |
|  |  |  |  |  | $\begin{aligned} & \pm(1.5 \%+10 \mathrm{cts}) \\ & 0,2 \leq \operatorname{Cos} \phi<0.8 \end{aligned}$ |  |
|  | $\begin{gathered} \text { AmpFLEX }{ }^{\text {m }} \\ \& \\ \text { Mini-AmpFLEX } \end{gathered}$ | 0 W | 9,999 kW | 4 digits | $\begin{gathered} \pm(1 \%) \\ \operatorname{Cos} \phi \geq 0.8 \end{gathered}$ |  |
|  |  |  |  |  | $\begin{aligned} & \pm(1.5 \%+10 \mathrm{cts}) \\ & 0.5 \leq \operatorname{Cos} \phi<0.8 \end{aligned}$ |  |
| Inductive \& capacitive reactive power values |  <br> Mini-AmpFLEX | 0 VAR | 9,999 kVAR | 4 digits | $\begin{gathered} \pm(1 \%) \\ \operatorname{Sin} \phi \geq 0.5 \end{gathered}$ |  |
|  |  |  |  |  | $\begin{gathered} \pm(1.5 \%+10 \mathrm{cts}) \\ 0.2 \leq \operatorname{Sin} \phi<0.5 \end{gathered}$ |  |
|  | $\begin{gathered} \text { AmpFLEX } \\ \& \in \\ \text { Mini-AmpFLEX } \end{gathered}$ | 0 VAR | 9,999 kVAR | 4 digits | $\begin{gathered} \pm(1.5 \%) \\ \operatorname{Sin} \phi \geq 0.5 \end{gathered}$ |  |
|  |  |  |  |  | $\begin{gathered} \pm(2.5 \%+20 \mathrm{cts}) \\ 0.2 \leq \operatorname{Sin} \phi<0.5 \end{gathered}$ |  |
| Apparent power |  | 0 VA | 9,999 kVA | 4 digits | $\pm$ (1 \%) |  |
| Power factor |  | -1 | 1 | 0.001 | $\begin{gathered} \pm(1.5 \%) \\ \cos \phi \geq 0,5 \end{gathered}$ |  |
|  |  | $\begin{aligned} & \pm(1.5 \%+10 \mathrm{cts}) \\ & 0.2 \leq \operatorname{Cos} \phi<0.5 \end{aligned}$ |  |  |  |  |

(1) Rating $1,000 \mathrm{~V}_{\text {RMs }}$ Category III, as long as the voltages between each of the terminals and the earth do not exceed $1,000 \mathrm{~V}_{\text {RMs. }}$
(2) With two-phase (opposing phases) - same remark as for (1).
(3) Caution: the absolute offset value must not exceed $95 \%$ of the peak amplitude

In other words, $\mathrm{s}(\mathrm{t})=\mathrm{S} \times \sin (\omega \mathrm{t})+\mathrm{O}$, so we will have $\mathrm{IOI} \leq 0.95 \times \mathrm{S}$ (with S positive).
The MAX and MIN values in the waveform mode and the $\mathrm{V}_{\text {RMS }}$ and $\mathrm{A}_{\text {RMS }}$ values (excluding neutral channels) in the Alarm and Inrush Current modes are half-period values.

## Note:

the uncertainties indicated for the power and energy measurements are maximum values for $\mid$ Cos $\phi \mid=1$ or $\operatorname{ISin} \phi I=1$ and are typical for the other phase shifts.

## Power \& Quality Analyser C.A 8335



## Power \& Quality Analyser C.A 8335

### 2.2.5 Specifications of the current sensors (after linearization)

The sensor errors are offset by typical correction inside the instrument. This typical correction is applied to the phase and the amplitude depending on the type of sensor connected (detected automatically) and the gain of the current acquisition line used.

The RMS current measurement error and the phase error correspond to additional errors (they must therefore be added to the instrument errors) indicated as influences on the calculations performed by the analyser (power values, energies, power factors, tangents, etc.).

| Sensor type | TRMS current | Maximum error on $\mathrm{I}_{\text {RMS }}$ | Maximum error on $\varphi$ |
| :---: | :---: | :---: | :---: |
| PAC93 clamp 1,000 A | [1A ; 10 A] | $\pm(1.5 \%+1 \mathrm{~A})$ | N.S. |
|  | [10 A ; 100 A ] |  | $\pm\left(2^{\circ}\right)$ |
|  | [100 A ; 800 A] | $\pm$ (3 \%) | $\pm\left(1.5^{\circ}\right)$ |
|  | [800 A ; 1,200 A] | $\pm(5 \%)$ |  |
| $\begin{aligned} & \text { C193 clamp } \\ & \text { 1,000 A } \end{aligned}$ | [1A ; 3 A] | $\pm(0.8$ \%) | N.S. |
|  | [3 A ; 10 A] |  | $\pm\left(1^{\circ}\right)$ |
|  | [10 A ; 100 A ] | $\pm(0.3$ \%) | $\pm\left(0.5^{\circ}\right)$ |
|  | [100 A ; 1,200 A] | $\pm(0.2$ \%) | $\pm\left(0.3^{\circ}\right)$ |
| $\begin{gathered} \text { AmpFLEX }{ }^{\text {TM }} \mathbf{A 1 9 3} \\ 6,500 \mathrm{~A} \end{gathered}$ | [10 A ; 100 A ] | $\pm(3$ \%) | $\pm\left(1^{\circ}\right)$ |
|  | [100 A ; 6,500 A] | $\pm(2 \%)$ | $\pm\left(0.5^{\circ}\right)$ |
| Mini-AmpFlex MA193 6,500 A | [10 A ; 100 A ] | $\pm$ (3 \%) | $\pm\left(1^{\circ}\right)$ |
|  | [100 A ; 6,500 A] | $\pm(2 \%)$ | $\pm\left(0.5^{\circ}\right)$ |
| MN93 clamp 200 A | [0.5 A ; 2 A] | $\pm(3 \%+1 \mathrm{~A})$ | N.S. |
|  | [2 A ; 10 A ] |  | $\pm\left(6^{\circ}\right)$ |
|  | [10 A ; 100 A ] | $\pm(2.5 \%+1 \mathrm{~A})$ | $\pm\left(3^{\circ}\right)$ |
|  | [100 A ; 240 A] | $\pm(1 \%+1 \mathrm{~A})$ | $\pm\left(2^{\circ}\right)$ |
| MN93A clamp 100 A | [100 mA ; 300 mA ] | $\pm(0.7 \%+2 \mathrm{~mA})$ | N.S. |
|  | [300 mA ; 1 A] |  | $\pm\left(1.5^{\circ}\right)$ |
|  | [1 A ; 120 A] | $\pm(0.7$ \%) | $\pm\left(0.7^{\circ}\right)$ |
| MN93A clamp 5 A | [ 5 mA ; 50 mA ] | $\pm(1 \%+0.1 \mathrm{~mA})$ | $\pm\left(1.7^{\circ}\right)$ |
|  | [ $50 \mathrm{~mA} ; 500 \mathrm{~mA}$ ] | $\pm(1 \%)$ | $\pm\left(1^{\circ}\right)$ |
|  | [500 mA ; 6 A ] | $\pm(0.7$ \%) |  |
| 5 A adapter | [ 5 mA ; 50 mA ] | $\pm(1 \%)$ | $\pm\left(1^{\circ}\right)$ |
|  | [50 mA ; 6 A] | $\pm(0.5$ \%) | $\pm\left(0^{\circ}\right)$ |

N.S. means "Not Specified"

## 3. FORMULAE

This chapter presents the mathematical formulae used to calculate the various parameters for the C.A 8335.

### 3.1 Mathematical formulae

### 3.1.1 Network frequency and sampling

The sampling is slaved to the network frequency to obtain 256 samples per period from 40 Hz to 70 Hz . This slaving is essential for calculation of the reactive power, unbalance, THD and harmonic angles.

The frequency measurement is determined by analysing seven consecutive positive zero crossings on the first voltage channel (V1) or on the first current channel (11) after digital low-pass filtering and digital suppression of the DC component.

Precise time measurement of the zero crossing point is carried out by linear interpolation between two samples to achieve a resolution better than $0.002 \%$.

The signals are acquired with a 16-bit converter and (for current acquisition) dynamic gain switching.
3.1.2 Half-period RMS values of the voltages and currents (excluding neutral)
Half-period RMS phase voltage of phase $i+1$
$\operatorname{Vhp}[i]=\sqrt{\frac{1}{N s a m H a l f P e r} \cdot} \cdot \sum_{n: Z \text { Zero }}^{\text {Nexteroro }} V[i][n]^{2}$
Half-period RMS composite voltage of phase i+1

$$
\operatorname{Uhp}[i]=\sqrt{\frac{1}{\text { NsamHalfPer }} \cdot \sum_{n: Z \text { Zero }}^{\text {Nexterero }} U[i][n]^{2}}
$$

Half-period RMS current of phase $\mathrm{i}+1$
$\operatorname{Ahp}[i]=\sqrt{\frac{1}{\text { NsamHalfPer }} \cdot \sum_{n: \text { Zero }}^{\text {Nexzero }} A[i][n]^{2}}$
Note: these values are calculated for each half-period to avoid missing any faults.

### 3.1.3 Minimum and maximum half-period RMS values (excluding neutral)

$$
\begin{aligned}
& \operatorname{Vmax}[i]=\max (\operatorname{Vhp}[i]), \quad \operatorname{Vmin}[i]=\min (\operatorname{Vhp}[i]) \\
& \operatorname{Umax}[i]=\max (\operatorname{Uhp}[i]), \quad \operatorname{Umin}[i]=\min (\operatorname{Uhp}[\mathrm{i}]) \\
& \operatorname{Amax}[i]=\max (\operatorname{Ahp}[i]), \operatorname{Amin}[i]=\min (\operatorname{Ahp}[i])
\end{aligned}
$$

### 3.1.4 Flicker for voltages (excluding neutral) <br> Method based on the IEC 61000-4-15 standard.

The input values are the half-period phase voltages. Blocks 3 and 4 are produced digitally. The classifier of block 5 comprises 128 levels.
The Vflk[i] values are updated every 10 minutes.

### 3.1.5 Peak values for voltages and currents

$\mathrm{i}=3 \Leftrightarrow$ neutral - except for Upp and Upm
$\mathrm{V}_{\mathrm{pp}}[\mathrm{i}]=\max (\mathrm{V}[i][\mathrm{n}]), \quad \mathrm{Vpm}[i]=\min (\mathrm{V}[i][\mathrm{n}]) \mathrm{n} \in[0 .$. NSAMPER - 1$]$
$\operatorname{Upp}[i]=\max (\mathrm{U}[\mathrm{i}][\mathrm{n}]), \quad \mathrm{Upm}[i]=\min (\mathrm{U}[i][\mathrm{n}]) \mathrm{n} \in[0 . .$. NSAMPER - 1$]$
$\operatorname{App}[i]=\max (\mathrm{A}[i][\mathrm{n}]), \operatorname{Apm}[i]=\min (\mathrm{A}[i][\mathrm{n}]) \mathrm{n} \in[0 .$. NSAMPER - 1$]$

### 3.1.6 Crest factors for voltages (excluding neutral)

Phase voltage crest factor of phase i+1


Composite voltage crest factor of phase i+1
$\operatorname{Ucf}[i]=\frac{\max (\mathrm{Upp}[\mathrm{i}], \mathrm{Upm}[\mathrm{i}])}{\sqrt{\frac{1}{\text { NSAMPER }} \cdot{ }^{\text {NSAMPER-1 }} \cdot \sum_{n=0} U[i][n]^{2}}}$
Current crest factor of phase i+1
$\operatorname{Acf}[i]=\frac{\max (\mathrm{App}[\mathrm{i}], \operatorname{Apm}[\mathrm{i}])}{\sqrt{\frac{1}{\text { NSAMPER }} \cdot{ }^{\text {NSAMPER-1 }} \sum_{n=0} A[i][n]^{2}}}$

### 3.1.7 1 s RMS values of voltages and currents

( $\mathrm{i}=3 \Leftrightarrow$ neutral - except for Urms)
RMS phase voltage $i+1$
$\operatorname{Vrms}[i]=\sqrt{\frac{1}{N S a m S e c} \cdot} \sum_{n=0}^{\text {NSamSec } V[i][n]^{2}}$

RMS composite voltage of phase $i+1$
$\operatorname{Urms}[i]=\sqrt{\frac{1}{N S a m S e c} \cdot} \cdot \sum_{n=0}^{\text {NSamSec }} U[i][n]^{2}$

RMS current of phase $i+1$
$\operatorname{Arms}[i]=\sqrt{\frac{1}{N S a m S e c} \cdot} \cdot \sum_{n=0}^{\text {NSamSec }} A[i][n]^{2}$
NSamSec: Number of samples per second

## Power \& Quality Analyser C.A 8335

### 3.1.8 Voltage and current unbalances

These are calculated from the filtered values (1s) VFrms and AFrms (ideally, the fundamental of the signals).
(vectorial operations by complex notation with: $a=e^{j \frac{2 \pi}{3}}$ )
Vrms $_{+}=\frac{1}{3}\left(\right.$ VFrms $\left.[0]+\mathrm{a} \cdot \operatorname{VFrms}[1]+\mathrm{a}^{2} \cdot \operatorname{VFrms}[2]\right)$ forward voltage
Vrms $=\frac{1}{3}\left(\right.$ VFrms $\left.[0]+\mathrm{a}^{2} \cdot \operatorname{VFrms}[1]+\mathrm{a} \cdot \operatorname{VFrms}[2]\right)$ reverse voltage
Vunb $=\frac{\mid \text { Vrms }_{-} \mid}{\mid \text {Vrms }_{+} \mid}$, Aunb $=\frac{\mid \text { Arms } \mid}{\mid \text { Arms }_{+} \mid}$

### 3.1.9 Harmonic calculations (excluding neutral)

These are performed by 1024-count FFT (16 bits) over four periods without windowing (see IEC 1000-4-7). On the basis of the real parts $b_{k}$ and imaginary parts $a_{k}$, the rates are calculated for each order and for each phase Vharm[3][51], Uharm[3][51] and Aharm[3][51] in relation to the fundamental value, and the angles $\mathrm{Vph}[3][51]$, Uph[3][51] and $\operatorname{Aph}[3][51]$ in relation to the fundamental.

The following principle is used for this calculation:
$\%$ modulus $\bmod _{k}=\frac{c_{k}}{c_{1}} \times 100$
Angle in degrees $\varphi_{k}=\arctan \left(\frac{a_{k}}{b_{k}}\right)$

$$
\text { with }\left\{\begin{array}{l}
c_{k}=\left|b_{k}+j a_{k}\right|=\sqrt{a_{k}^{2}+b_{k}^{2}} \\
b_{k}=\frac{1}{512} \sum_{s=0}^{1024} F_{s} \times \sin \left(\frac{k \pi}{512} s+\varphi_{k}\right) \\
a_{k}=\frac{1}{512} \sum_{s=0}^{1024} F_{s} \times \cos \left(\frac{k \pi}{512} s+\varphi_{k}\right) \\
c_{0}=\frac{1}{1024} \sum_{s=0}^{1024} F_{s}
\end{array}\right.
$$

$\mathrm{C}_{\mathrm{k}}$ : amplitude of the component with a frequency $f_{k}=\frac{k}{4} f_{1}$
$\mathrm{F}_{\mathrm{s}}$ : signal sampled
$\mathrm{C}_{0}$ : DC component
K: ordinal number (order of the spectrum line)

### 3.1.10 Harmonic distortion (excluding neutral)

Two global values are calculated which indicate the relative quantity of harmonics: the THD as a proportion of the fundamental and the DF as a proportion of the RMS value



By multiplying the voltage THDs by the current THDs, the power THDs can be calculated. By differentiating the voltage harmonic angles with the current harmonic angles, the power harmonic angles can be calculated.

VAharm[3][51], VAph[3][51]

### 3.1.11 Facteur K

Facteur K pour la phase i+1
$\operatorname{Akf}[\mathrm{i}]=\frac{\sum_{n=1}^{n=50} n^{2} \cdot \operatorname{Aharm}[i][n]^{2}}{\sum_{n=1}^{n=50} \text { Aharm }[i][n]^{2}}$

### 3.1.12 Different 1 s power values (excluding neutral)

Active power, phase $i+1$
$\mathrm{W}[i]=\frac{1}{N \operatorname{SamSec}} \cdot \sum_{n=0}^{\text {NSamSec-1 }} V[i][n] \cdot A[i][n]$

Apparent power, phase i+1
$\operatorname{VA}[i]=\operatorname{Vrms}[i] \cdot \operatorname{Arms}[i]$

Reactive power, phase i+1
$\operatorname{VAR}[i]=\frac{1}{N S a m S e c} \cdot \sum_{n=0}^{\text {NSamsec-1 }} V F[i][n-N S A M P E R / 4] \cdot A F[i][n]$
or $\operatorname{VAR}[\mathrm{i}]=\sqrt{\mathrm{VA}[i]^{2}-\mathrm{W}[i]^{2}}$ if using the calculation method with harmonics.

The reactive power values are calculated using the filtered signals (without harmonics), as required by EDF, or on the basis of the apparent and active power values (with harmonics). The calculation method is chosen by the user.

Total active power
$\mathrm{W}[3]=\mathrm{W}[0]+\mathrm{W}[1]+\mathrm{W}[2]$
Total apparent power
$\mathrm{VA}[3]=\mathrm{VA}[0]+\mathrm{VA}[1]+\mathrm{VA}[2]$
Total reactive power
$\operatorname{VAR}[3]=\operatorname{VAR}[0]+\operatorname{VAR}[1]+\operatorname{VAR}[2]$

## Power \& Quality Analyser C.A 8335

### 3.1.13 Different rates (excluding neutral)



Power factor, phase $\mathrm{i}+1$
$\operatorname{DPF}[i]=\cos (\phi[i])$
$\operatorname{Tan}[\mathrm{i}]=\tan (\phi[i])$
Displacement power factor, phase i +1
Tangent phase i+1
Cosine of angle between voltage fundamental and current fundamental, phase i + 1

$\mathrm{PF}[3]=\frac{\mathrm{PF}[0]+\mathrm{PF}[1]+\mathrm{PF}[2]}{3}$
Total power factor
$\operatorname{DPF}[3]=\frac{\mathrm{DPF}[0]+\mathrm{DPF}[1]+\mathrm{DPF}[2]}{3}$
Total displacement power factor
$\operatorname{Tan}[3]=\frac{\operatorname{Tan}[0]+\operatorname{Tan}[1]+\operatorname{Tan}[2]}{3}$
Total tangent

### 3.1.14 Different energy values (excluding neutral)

- Case 1: consumed energy values ( $\mathrm{W}[\mathrm{i}] \geq 0$ )

Consumed active energy, phase $i+1$
$\mathrm{Wh}[0][i]=\sum_{\text {Tint }} \frac{W[i]}{3600}$
Consumed apparent energy, phase $i+1$
$\operatorname{VAh}[0][i]=\sum_{\text {Tint }} \frac{V A[i]}{3600}$
Consumed inductive reactive energy, phase i+1
$\operatorname{VARhL}[0][i]=\sum_{\text {Tint }} \frac{V A R[i]}{3600}$ for $\operatorname{VAR}[\mathrm{i}] \geq 0$
Consumed capacitive reactive energy, phase $i+1$
$\operatorname{VARhC}[0][i]=\sum_{\text {Tint }} \frac{-V A R[i]}{3600}$ for $\operatorname{VAR}[\mathrm{i}] \leq 0$
Total consumed active energy
$\mathrm{Wh}[0][3]=\mathrm{Wh}[0][0]+\mathrm{Wh}[0][1]+\mathrm{Wh}[0][2]$

Total consumed apparent energy
$\operatorname{VAh}[0][3]=\operatorname{VAh}[0][0]+\operatorname{VAh}[0][1]+\operatorname{VAh}[0][2]$
Total consumed capacitive reactive energy
VARhC[0][3] = VARhC[0][0] + VARhC[0][1] + VARhC[0][2]

Total consumed inductive reactive energy
$\operatorname{VARhL}[0][3]=$ VARhL[0][0] $+\operatorname{VARhL[0][1]~+~VARhL[0][2]~}$

- Case 2: generated energy values ( $\mathrm{W}[\mathrm{i}]<0$ )

Generated active energy, phase $i+1$
$\mathrm{Wh}[1][i]=\sum_{\text {Tint }} \frac{W[i]}{3600}$

Generated apparent energy, phase $i+1$
$\operatorname{VAh}[1][i]=\sum_{\text {Tint }} \frac{V A[i]}{3600}$

Generated inductive reactive energy, phase $i+1$
$\operatorname{VARhL}[1][i]=\sum_{\text {Tint }} \frac{-V A R[i]}{3600}$ for $\operatorname{VAR}[\mathrm{i}] \leq 0$

Generated capacitive reactive energy, phase i+1
$\operatorname{VARhC}[1][i]=\sum_{\text {Tint }} \frac{V A R[i]}{3600}$ for $\operatorname{VAR}[\mathrm{i}] \geq 0$

Total generated active energy
$\mathrm{Wh}[1][3]=\mathrm{Wh}[1][0]+\mathrm{Wh}[1][1]+\mathrm{Wh}[1][2]$

Total generated apparent energy
$\operatorname{VAh}[1][3]=\operatorname{VAh}[1][0]+\operatorname{VAh}[1][1]+\operatorname{VAh}[1][2]$

Total generated capacitive reactive energy
VARhC[1][3] = VARhC[1][0] + VARhC[1][1] + VARhC[1][2]

## Total generated inductive reactive energy

$\operatorname{VARhL}[1][3]=\operatorname{VARhL}[1][0]+\operatorname{VARhL}[1][1]+\operatorname{VARhL}[1][2]$

### 3.2 Hysteresis

Hysteresis is a filtering principle frequently used after a threshold detection stage, in Alarm mode $\triangle$
Correct adjustment of the hysteresis value prevents repeated status changes when the measurement oscillates around the threshold.

### 3.2.1 Overvoltage detection

For a hysteresis of $2 \%$, for example, the return level for an overvoltage detection will be equal to ( $100 \%-2 \%$ ), or $98 \%$ of the reference threshold voltage.


### 3.2.2 Detection of undervoltage or interruption

For a 2 \% hysteresis, for example, the return level in the event of undervoltage detection will be equal to (100 \% $+2 \%$ ) or $102 \%$ of the threshold voltage Uref.


## Power \& Quality Analyser C.A 8335

### 3.3 Minimum scale values and minimum displayed values in the Waveforms mode

| Type of current sensor | Minimum displayed current value $[\mathrm{A}]$ | Minimum scale current value $[\mathrm{A}]$ |
| :---: | :---: | :---: |
| AmpFLE $\boldsymbol{X}^{\text {TM }} 6500 \mathrm{~A}$ | 30 | 60 |
| Mini-AmpFLEX 6500 A | 30 | 60 |
| PAC93 1,000 A clamp | 1 | 10 |
| C193 1,000 A clamp | 0.5 | 10 |
| MN93 200 A clamp | 0.5 | 2 |
| MN93A 100 A clamp | 0.2 | 1 |
| MN93A clamp with 5 A probe | (Primary $\times 5) \div($ Secondary $\times 1,000)$ | (Primary $\times 5 \times 10) \div($ Secondary $\times 1,000)$ |
| 5 A adapter | (Primary $\times 5) \div($ Secondary $\times 1,000)$ | (Primary $\times 5 \times 10) \div($ Secondary $\times 1,000)$ |

### 3.4 Diagram of the 4 quadrants

This diagram is used for power and energy measurements V


### 3.5 Half-tube values for transient capture

| Threshold | 100 \% | 50 \% | 20 \% | 10 \% | 5 \% | 2 \% | 1 \% | Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Half-width of tube (L) | 200 | 100 | 40 | 20.01 | 10 | 4 | 2 | MN93 200 A |
|  | 100 | 50 | 20 | 10 | 5 | 2 | 1 | MN93A 100 A |
|  | 3,000 | 1,500 | 600 | 300 | 150 | 60 | 30 | MN93A 5 A / 5 A adapter [3,000 / 1] |
|  | 1 | 0.5 | 0.2 | 0.1 | 0.05 | 0.02 | 0.01 | MN93A 5 A / 5 A adapter [1/1] |
|  | 1,000 | 500 | 200 | 100 | 50 | 20 | 10 | PAC93 1,000 A |
|  | 3,000 | 1,500 | 600 | 300 | 150 | 60 | 30 | AmpFLEX ${ }^{\text {TM }} / \mathbf{M i n i - A m p F L E X ~} 3,000 \mathrm{~A}$ |
|  | 500 | 250 | 100 | 50 | 25 | 10 | 5 | Voltage 500 V |

# We are supporting you to deliver a world class service, every day, in every sector... 

## LOCATIONS

## LONDON, HEATHROW

Sunbelt Rentals UK Test \& Monitoring
242-252 London Road, Staines, London TW18 4JQ 03331223126
www.sunbeltrentals.co.uk/find-a-depot/london-heathrow

## REDCAR

Sunbelt Rentals UK Test \& Monitoring
Unit 5 Kirkleatham Business Park, Redcar TS10 5SQ 03703306021
www.sunbeltrentals.co.uk/find-a-depot/teesside

## STOKESLEY

Sunbelt Rentals UK Test \& Monitoring
2 Ellerbeck Way, Stokesley Business Park, Stokesley, North Yorkshire TS9 5JZ
01642718900
www.sunbeltrentals.co.uk/find-a-depot/stokesley

www.inlec.com
Order Online with Next Day Delivery, Online Chat \& Online Account Management

View our trustpilot score


